

# Modified-atmosphere Packaging of Blueberry Fruit: Effect of Temperature on Package O<sub>2</sub> and CO<sub>2</sub>

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**Abstract.** Highbush blueberry (*Vaccinium corymbosum* L. ‘Bluecrop’) fruit sealed in low-density polyethylene packages were incubated at 0, 5, 10, 15, 20, or 25C until O<sub>2</sub> and CO<sub>2</sub> levels in the package reached a steady state. A range of steady-state O<sub>2</sub> partial pressures (1 to 18 kPa) was created by placing a range of fruit weights within packages having a constant surface area and film thickness. The steady-state O<sub>2</sub> partial pressure in packages containing the same weight of fruit decreased as temperature increased, indicating the respiratory rate rose more rapidly (i.e., had a greater sensitivity to temperature) than O<sub>2</sub> transmission through the film. Steady-state O<sub>2</sub> and CO<sub>2</sub> partial pressures were used to calculate rates of O<sub>2</sub> uptake, CO<sub>2</sub> production, and the respiratory quotient (RQ). The effects of temperature and O<sub>2</sub> partial pressure on O<sub>2</sub> uptake and CO<sub>2</sub> production and the RQ were characterized. The steady-state O<sub>2</sub> partial pressure at which the fruit began to exhibit anaerobic CO<sub>2</sub> production (the RQ breakpoint) increased with increasing temperature, which implies that blueberry fruit can be stored at lower O<sub>2</sub> partial pressures when stored at lower temperatures.

Studies using controlled-atmosphere (CA) storage techniques have indicated that shelf-life extension can be obtained for blueberry (*Vaccinium* spp.) fruit using combinations of elevated CO<sub>2</sub> and reduced O<sub>2</sub> in the storage environment (Ceponis and Cappellini, 1985; Smittle and Miller, 1988). CA storage of highbush blueberry fruit is now a commercial reality and current conditions range from 1.5 to 2.5 kPa O<sub>2</sub> (1% O<sub>2</sub> = 1.013 kPa O<sub>2</sub> at 1 atm) and 5 to 12 kPa CO<sub>2</sub> at 0C.

Present-day commercial techniques for packaging blueberry fruit do not modify O<sub>2</sub> and CO<sub>2</sub> to levels that would enhance storage. Modified-atmosphere packaging (MAP) has the potential to provide low O<sub>2</sub>/high CO<sub>2</sub> regimes similar to those of CA storage, but throughout the marketing chain. Ideally, a package should maintain the appropriate atmospheric composition over the range of temperatures commonly encountered between harvest and consumption. Poor temperature control, however, can cause package O<sub>2</sub> levels to drop low enough to induce anaerobic respiration (Kader et al., 1989).

The purpose of our work was to investigate the influence of temperature on package O<sub>2</sub> and CO<sub>2</sub> partial pressures, on the rates of O<sub>2</sub> uptake and CO<sub>2</sub> production as functions of package O<sub>2</sub> partial pressure, and on the O<sub>2</sub> partial pressure at the RQ breakpoint. Blueberry fruit were chosen for investigation due to their relatively long shelf life, their minimal changes in respiration associated with ripening, and their relative insensitivity to CO<sub>2</sub> levels over the range of those expected to be encountered in the packaging system used.

## Materials and Methods

### Plant material

Fruit of ‘Bluecrop’ were hand-harvested into 46 × 61 × 20-cm plastic field lugs (≈ 8 kg of fruit) on 17 Aug. 1989 (second

harvest of the season) in the West Olive area of Michigan. Fruit were transported immediately to East Lansing in ice chests. Fruit were held overnight at 5C, sorted for obvious defects, and packaged the next morning.

### Film permeability

The permeability of 0.00495 cm (2 mil) low-density polyethylene (LDPE) film to O<sub>2</sub> and CO<sub>2</sub> was determined three to 15 times for each of three random samples at temperatures ranging from 0 to 35C at 5C intervals. It was important to obtain our own permeability coefficients, since values supplied by manufacturers are often inaccurate. Film permeability values vary with each production run for a particular film type, and, in fact, we have commonly found a 10% to 15% variation in permeability along the length of a single roll of film.

The various temperatures were established by submersing a specially built aluminum permeability cell in a water bath (Lauda RC20; Brinkman Instrument Co., West Bury, N.Y.), and temperature (± 0.1C) was verified using mercury and thermocouple thermometers. The permeability cell contained two circular (8 cm diameter × 0.5 cm deep) 25-ml chambers separated by the film sample, of which 50 cm<sup>2</sup> was exposed to both chambers and sealed in place by an O-ring. The permeability cell was fitted with a 3.5-m coil of 0.64-cm (id.) copper tubing on the gas inlets to permit the inlet gas to reach the temperature of the water bath before entering the cell. Pure O<sub>2</sub>, pure CO<sub>2</sub>, or a mixture of both gases was introduced to one chamber of the cell and an N<sub>2</sub> carrier gas was introduced to the other chamber. The rate of O<sub>2</sub> and CO<sub>2</sub> diffusion through the film was calculated from the steady-state partial pressure of the sample gases diffusing through the film and into the carrier gas stream. The partial pressure of O<sub>2</sub> and/or CO<sub>2</sub> in the carrier gas stream was determined using a sequential combination of O<sub>2</sub> (Ametek S-3A/II with a calcia-zirconia electrochemical detection cell; Ametek Co., Thermox Instrument Div., Pittsburgh) and CO<sub>2</sub> (ADC 225-MK3 analytical infrared gas analyzer; Analytical Development Co., Hertfordshire, England) analyzers. Gas concentrations in

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Abbreviations: CA, controlled atmosphere; LDPE, low-density polyethylene; MAP, modified-atmosphere packaging; RQ, respiratory quotient.

the carrier gas ranged from 2.5 to 150  $\mu\text{l O}_2/\text{liter}$  and 12.5 to 750  $\mu\text{l CO}_2/\text{liter}$ , which were well within the limits of detectability. Concentrations were calculated relative to a certified standard gas mixture (109  $\mu\text{l O}_2/\text{liter}$  and 94.3  $\mu\text{l CO}_2/\text{liter}$  in  $\text{N}_2$  gas). Flow rates were maintained at 100  $\text{ml}\cdot\text{min}^{-1}$  for all gases, and the chamber pressures were equalized and maintained at  $\approx 6$  cm  $\text{H}_2\text{O}$  above atmospheric.

Calculated concentrations were converted to partial pressures for determination of permeability coefficients. A best-fit equation of an Arrhenius plot of the data was used to determine permeability coefficients for packages at each storage temperature.

### Packaging

Blueberry fruit were sealed into 10  $\times$  20-cm (400  $\text{cm}^2$  total surface area) pouches comprised of 0.00495-cm-thick LDPE film (DOW Chemical Co., Midland, Mich.) for which  $\text{O}_2$  and  $\text{CO}_2$  permeability was measured as described above. Each package was equipped with a gas-sampling septum constructed of a short strip of electrical tape with a dab of DuPont Silicone II tub/tiling glue and sealant (Boylan-Pett, 1986). Fruit were weighed before being packaged, and weight per package was targeted at the following: 10, 20, 30, 40, 50, 60, 70, 80, 90, 110, 130, and 150 g. This range of 12 target weights was designed to generate a nearly continuous range of steady-state  $\text{O}_2$  and  $\text{CO}_2$  partial pressures within the package (Cameron et al., 1989). This range of fruit weights was placed at 0, 5, 10, 15, 20, and 25°C with four packages at each target weight/temperature combination.

### Steady-state $\text{O}_2$ and $\text{CO}_2$ levels and respiratory rates

Package gas composition was determined daily by withdrawing a 1-ml gas sample from the package with an insulin-type plastic syringe and analyzing the sample for  $\text{O}_2$  and  $\text{CO}_2$  using the above-noted  $\text{O}_2$  and  $\text{CO}_2$  analyzers connected in series with  $\text{N}_2$  as the carrier gas (flow rate = 150 to 200  $\text{ml}\cdot\text{min}^{-1}$ ). With this arrangement of detectors,  $\text{O}_2$  and  $\text{CO}_2$  concentrations could be determined for the same gas sample in  $\approx 10$  sec and there was no need to correct for argon as in conventional gas chromatography. As before, gas concentrations were converted to partial pressures. The gas composition of individual packages was monitored until steady-state conditions were reached, at which time data were collected and analyzed. The time needed to achieve steady-state conditions increased as the storage temperature decreased and ranged from 2 days at 25°C to  $\approx 14$  days at 0. No fungicide treatment was used; data were not taken from packages having obvious holes or containing moldy berries.

The steady-state  $\text{O}_2$  and  $\text{CO}_2$  partial pressures of the packages and the permeability data were combined to ascertain the rates of respiration using the following formulae:

$$RR_{\text{O}_2} = \frac{P_{\text{O}_2} \cdot A}{x} [(O_2)_{\text{atm}} - (O_2)_{\text{pkg}}] \quad [1]$$

$$RR_{\text{CO}_2} = \frac{P_{\text{CO}_2} \cdot A}{x} [(CO_2)_{\text{pkg}} - (CO_2)_{\text{atm}}], \quad [2]$$

where  $RR_{\text{O}_2}$  and  $RR_{\text{CO}_2}$  are the rates of  $\text{O}_2$  uptake and  $\text{CO}_2$  production ( $\text{mmol}\cdot\text{kg}^{-1}\cdot\text{h}^{-1}$ ), respectively;  $P_{\text{O}_2}$  and  $P_{\text{CO}_2}$  are mea-

sured  $\text{O}_2$  and  $\text{CO}_2$  permeability coefficients ( $\text{mmol}\cdot\text{cm}^{-1}$  per  $\text{cm}^2$  per hour per kPa), respectively, for our LDPE at the storage temperature;  $A$  is film area ( $\text{cm}^2$ );  $x$  is film thickness (cm);  $(O_2)_{\text{atm}}$  and  $(O_2)_{\text{pkg}}$  are atmospheric and package partial pressures of  $\text{O}_2$  (kPa), respectively;  $(CO_2)_{\text{pkg}}$  and  $(CO_2)_{\text{atm}}$  are the package and atmospheric  $\text{CO}_2$  partial pressures (kPa), respectively, and  $W$  is fruit weight (kg). The RQ was calculated as  $RR_{\text{CO}_2}$ , divided by  $RR_{\text{O}_2}$ . Data were plotted and analyzed using a computer nonlinear regression analysis package (Eisensmith, 1987).

## Results

### Film permeability

$P_{\text{O}_2}$  and  $P_{\text{CO}_2}$  increased exponentially with increasing temperature (Fig. 1). An Arrhenius plot of the data (Fig. 1, inset) indicated that the natural log of the permeability coefficient for both gases depended linearly on the reciprocal of temperature ( $^{\circ}\text{K}$ ), and the relationship could be expressed with the equation:

$$\ln(P_i) = \frac{E_a}{RT} + \ln(A), \quad [3]$$

where  $P_i$  is  $P_{\text{O}_2}$  or  $P_{\text{CO}_2}$ ;  $E_a$  is the energy of activation of  $\text{O}_2$  or  $\text{CO}_2$  permeation ( $\text{kJ}\cdot\text{mol}^{-1}$ ); and  $R$  is the gas constant (0.0083144  $\text{kJ/mol per } ^{\circ}\text{K}$ ). The slope of the fitted line was  $E_a/R$ . Average  $E_a$  values were 39.72  $\text{kJ}\cdot\text{mol}^{-1}$  for  $\text{O}_2$  ( $SD = 1.3$ ) and 35.53  $\text{kJ}\cdot\text{mol}^{-1}$  for  $\text{CO}_2$  ( $SD = 0.31$ ). Average values for the  $Y$  intercept [ $\ln(A)$ ] were 5.42 for  $\text{O}_2$  ( $SD = 0.13$ ) and 5.22 for  $\text{CO}_2$  ( $SD = 0.027$ ). The coefficient of determination ( $r^2$ ) values for individual  $E_a/R$  determinations ranged from 0.9951 to 0.9999 for  $\text{O}_2$  and 0.9984 to 0.9999 for  $\text{CO}_2$ . Values obtained for  $E_a$  and permeability coefficients are similar to published values for LDPE (Yasuda and Stannett, 1975). Equations for predicting  $P_{\text{O}_2}$  and  $P_{\text{CO}_2}$  for the film at any  $T$  are as follows:

$$P_{\text{O}_2} = 0.2269 \times \exp(-4777/T) \text{ mmol}\cdot\text{cm}^{-1} \text{ per cm}^2 \text{ per hour per kPa} \quad [4]$$

$$P_{\text{CO}_2} = 0.1858 \times \exp(-4273/T) \text{ mmol}\cdot\text{cm}^{-1} \text{ per cm}^2 \text{ per hour per kPa}, \quad [5]$$

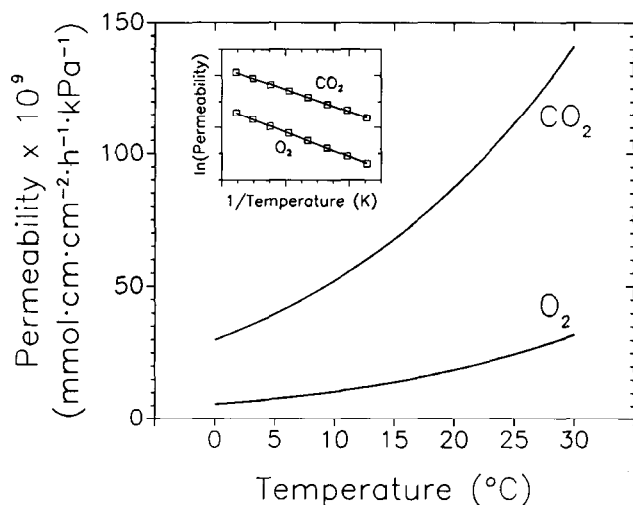


Fig. 1. Effect of temperature on film permeability constants for  $\text{O}_2$  and  $\text{CO}_2$  ( $P_{\text{O}_2}$  and  $P_{\text{CO}_2}$ , respectively) for 0.00495-cm-thick LDPE film used in packaging experiments. Inset: Arrhenius plot of  $\text{O}_2$  and  $\text{CO}_2$  permeability for typical film sample.

where T is temperature in °K. Values of  $PO_2 \cdot A/x$  and  $PCO_2 \cdot A/x$  were generated using Eq. [4] and [5] and substituting 400 cm<sup>2</sup> and 0.00495 cm for A and x, respectively (Table 1). These values and weight vs. O<sub>2</sub> and CO<sub>2</sub> data from Fig. 2 can be substituted directly into Eq. [1] and [2] for calculation of  $RR_{O_2}$  and  $RR_{CO_2}$  for any one of the six temperatures studied.  $PCO_2$  was ≈4.5 to 5 times  $PO_2$  for this film over the temperature range (Table 1).

### Steady-state O<sub>2</sub> and CO<sub>2</sub> levels and respiratory rates

Increasing the weight of fruit in the package caused a decrease in steady-state O<sub>2</sub> at each temperature (Fig. 2). As the temperature increased, steady-state O<sub>2</sub> tended to decrease for a given package fruit weight (Fig. 3). The data describing the relation-

Table 1. Whole package O<sub>2</sub> and CO<sub>2</sub> permeabilities ( $PO_2 \cdot A/x$  and  $PCO_2 \cdot A/x$ , respectively) for the packages used in these experiments at 0, 5, 10, 15, 20, and 25°C. Values were generated using Eqs. [4] and [5] for packages having a surface area (A) of 400 cm<sup>2</sup> and film thickness (x) of 0.00495 cm.  $PO_2$  and  $PCO_2$  are LDPE film permeability constants for O<sub>2</sub> and CO<sub>2</sub>, respectively. Eq. [4]:  $PO_2 = 0.2269 \times \exp(-4777/T)$  mmol·cm<sup>-1</sup> per cm<sup>2</sup> per hour per kPa; and Eq. [5]:  $PCO_2 = 0.1858 \times \exp(-4273/T)$  mmol·cm<sup>-1</sup> per cm<sup>2</sup> per hour per kPa.

Temp (°C)	$PO_2 \cdot A/x$ (mmol·h <sup>-1</sup> ·kPa <sup>-1</sup> )	$PCO_2 \cdot A/x$	$PCO_2/PO_2$
0	$4.612 \times 10^{-4}$	$2.393 \times 10^{-3}$	5.19
5	$6.318 \times 10^{-4}$	$3.171 \times 10^{-3}$	5.01
10	$8.560 \times 10^{-4}$	$4.160 \times 10^{-3}$	4.86
15	$11.47 \times 10^{-4}$	$5.407 \times 10^{-3}$	4.71
20	$15.23 \times 10^{-4}$	$6.965 \times 10^{-3}$	4.57
25	$20.02 \times 10^{-4}$	$8.896 \times 10^{-3}$	4.44

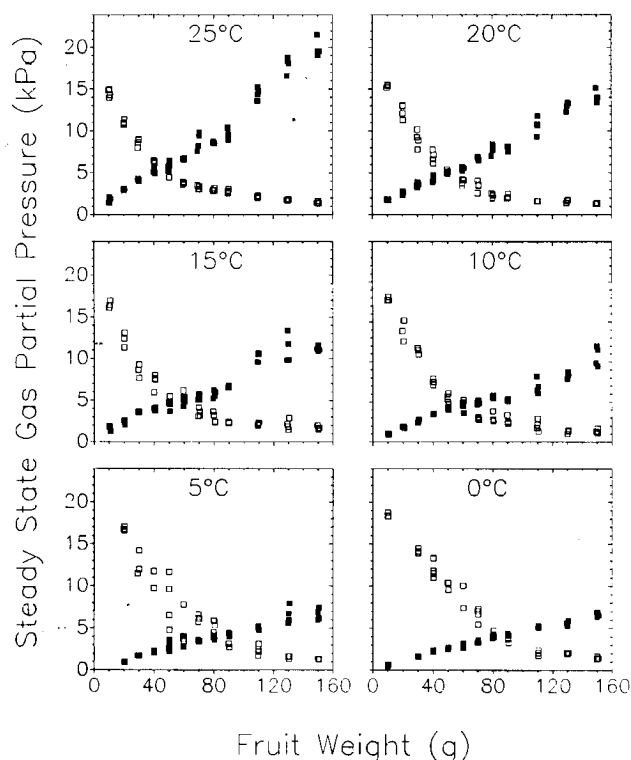


Fig. 2. Effect of blueberry fruit weight on steady-state O<sub>2</sub> (open symbols) and CO<sub>2</sub> (closed symbols) partial pressures in 400-cm<sup>2</sup>, 0.00495-cm-thick LDPE sealed packages held at 0, 5, 10, 15, 20, or 25°C.

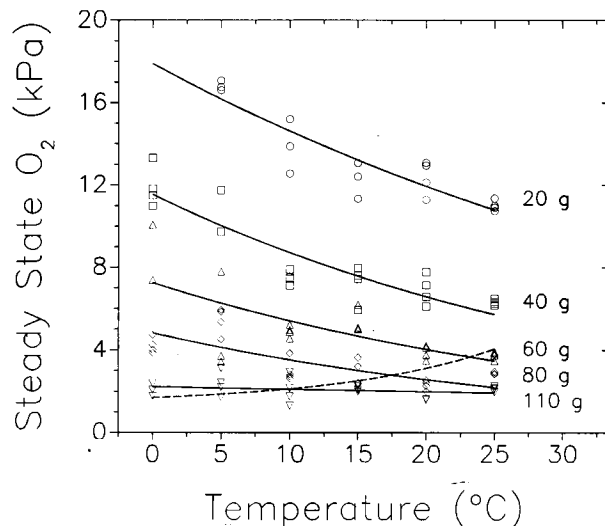


Fig. 3. Effect of temperature on: 1) steady-state O<sub>2</sub> levels for various weights of blueberry fruit sealed in 400-cm<sup>2</sup>, 0.00495-cm-thick LDPE packages (solid lines) containing 20, 40, 60, 80, or 110 g of fruit; and 2) the estimated lower O<sub>2</sub> limit for blueberry fruit (dashed line) based on Fig. 6. See Table 2 for equations describing curves.

Table 2. General equation (Eq. [2]) and values of weight-dependent constants describing the relationship between temperature (°C) and steady-state O<sub>2</sub> partial pressures (kPa) for various weights of blueberry fruit sealed in LDPE pouches and stored at six temperatures. Eq. [2]:  $(O_2)_{pkg} = x_1 \cdot \exp(-x_2 \cdot T)$ .

Package wt (g)	$x_1$	$x_2$	$R^2$
20	17.89	$2.02 \times 10^{-2}$	0.82
40	11.54	$2.81 \times 10^{-2}$	0.82
60	7.248	$2.94 \times 10^{-2}$	0.48
80	4.816	$3.14 \times 10^{-2}$	0.52
110	2.218	$5.66 \times 10^{-3}$	0.05

ship between fruit temperature and package O<sub>2</sub> were fitted empirically with the simple exponential equation:

$$(O_2)_{pkg} = x_1 \cdot \exp(x_2 \cdot T), \quad [6]$$

where  $(O_2)_{pkg}$  is the steady-state O<sub>2</sub> partial pressure and T is temperature in °C. Values for weight-dependent constants  $x_1$  and  $x_2$  and the  $R^2$  of the fit are listed in Table 2.

The measured O<sub>2</sub> and CO<sub>2</sub> gradients across the film were used to calculate steady-state diffusion rates for both gases through the film, and the respiration rates were calculated (assuming diffusion rates through the package were equal to O<sub>2</sub> and CO<sub>2</sub> fluxes for the respiratory processes) on a per-package weight basis. For each temperature, the relationship between O<sub>2</sub> uptake and steady-state O<sub>2</sub> (Fig. 4) was empirically fitted with the exponential equation:

$$RR_{O_2} = b_1 \{ 1 - \exp[-b_2 \cdot (O_2)_{pkg}] \}^{b_3} \quad [7]$$

(Cameron, 1990; Cameron et al., 1989), where  $RR_{O_2}$  is the rate of O<sub>2</sub> uptake (mmol·kg<sup>-1</sup>·h<sup>-1</sup>) and  $(O_2)_{pkg}$  is the steady-state O<sub>2</sub> partial pressure (kPa). Values for constants  $b_1$ ,  $b_2$ , and  $b_3$  and the  $R^2$  of the fit at each temperature are listed in Table 3.

Oxygen consumption decreased in response to decreasing temperature and decreasing steady-state O<sub>2</sub> (Fig. 4). Interestingly, the shape of the O<sub>2</sub>-dependent respiratory curves changed with temperature. At the higher temperatures, O<sub>2</sub> uptake did not appear to approach saturation even at the highest levels of steady-

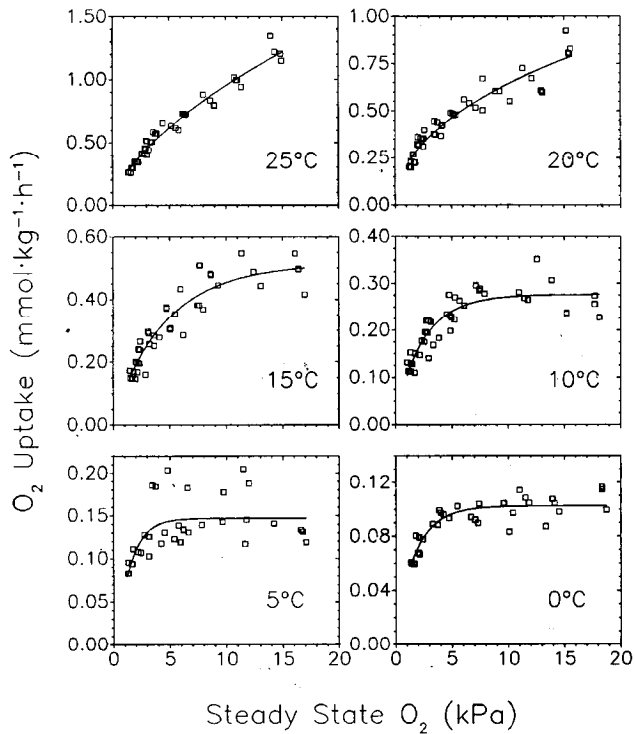


Fig.4. Interdependent effects of steady-state  $O_2$  partial pressure and storage temperature on the calculated rate of  $O_2$  uptake of blueberry fruit in sealed LDPE packages. See Table 4 for equations describing curves.

Table 3. General equation (Eq. [7]) and values of temperature-dependent constants describing the relationship between steady-state  $O_2$  partial pressures (kPa) and  $O_2$  uptake ( $mmol \cdot kg^{-1} \cdot h^{-1}$ ) for blueberry fruit sealed in LDPE Douches and stored at various temperatures. Eq. [7]:  $RR_{O_2} = b_1 \cdot \{1 - \exp[-b_2 \cdot (O_2)_{pk}]\}^{b_3}$ .

Temp (°C)	$b_1$	$b_2$	$b_3$	$R^2$
25	4.561	$9.111 \times 10^{-3}$	0.6428	0.97
20	1.871	$1.235 \times 10^{-2}$	0.4968	0.92
15	0.514	$2.067 \times 10^{-1}$	0.9205	0.88
10	0.2765	$3.829 \times 10^{-1}$	0.8795	0.81
5	0.1469	$8.461 \times 10^{-1}$	1.401	0.48
0	0.1024	$5.427 \times 10^{-1}$	0.8506	0.80

state  $O_2$  generated. As temperature declined, however,  $O_2$  uptake showed signs of saturation at ever decreasing  $O_2$  partial pressures. As a result of this phenomenon, fruit were found to be more sensitive to restricted  $O_2$  availability as temperatures increased. For instance, at 0C respiration at 1.5 kPa  $O_2$  was about half that at 16 kPa  $O_2$ , while at 25C, respiration at 1.5 kPa  $O_2$  was about one-fifth that at 16 kPa (Fig. 4).

Carbon dioxide production depended on temperature and  $O_2$  partial pressure (Fig. 5). Carbon dioxide production declined with decreasing temperature and, in general, with decreasing  $O_2$  levels. At the lower  $O_2$  partial pressures, however, the  $CO_2$  respiratory rate did not approach zero, and at some temperatures,  $CO_2$  production increased as the  $O_2$  partial pressures decreased. The rate of  $CO_2$  production was not fitted with an equation due to the difficulties presented by the inflection in the data occurring at the lower  $O_2$  levels.

The RQ depended on both steady-state  $O_2$  and storage temperature (Fig. 6). At all temperatures except 0C, the RQ increased as the steady-state  $O_2$  approached zero; however, the RQ breakpoint occurred at higher levels of  $O_2$  as temperature

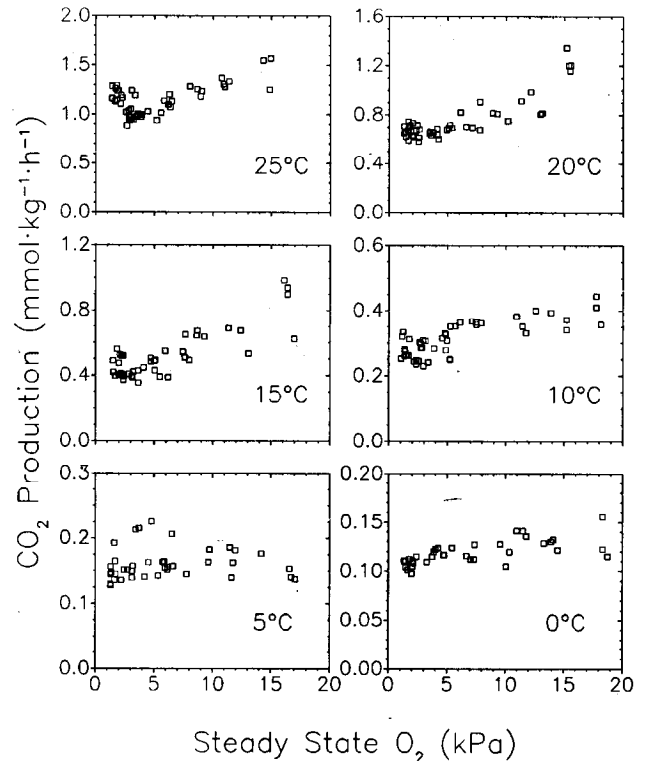


Fig. 5. Interdependent effects of steady-state  $O_2$  partial pressure and storage temperature on calculated rate of  $CO_2$  production of blueberry fruit in sealed LDPE packages.

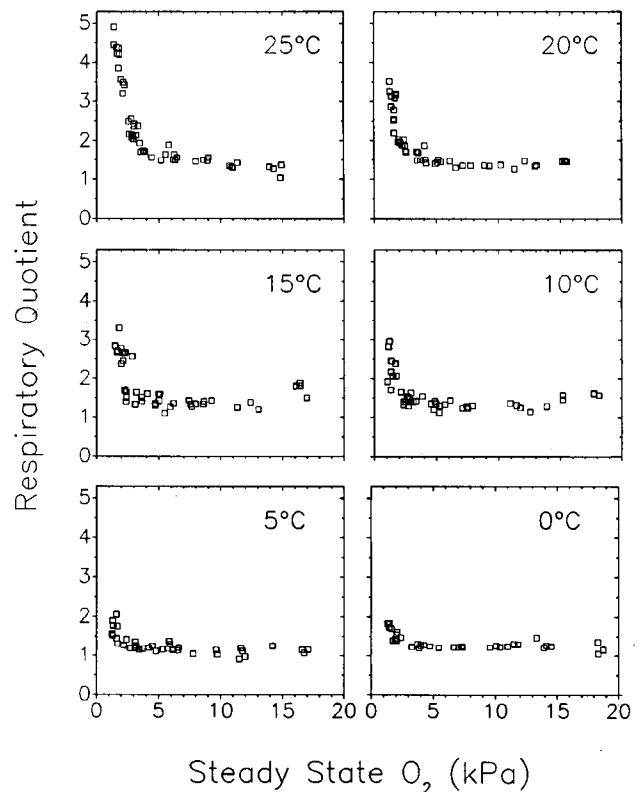


Fig. 6. Effect of steady-state  $O_2$  partial pressure on the respiratory quotient of blueberry fruit in sealed LDPE packages held at 0, 5, 10, 15, 20, or 25C.

increased. Estimates of the  $O_2$  partial pressure at which the RQ breakpoint occurred were made from the graphs: 1.8 kPa at 5C; 2.0 kPa at 10C; 2.5 kPa at 15C; 3.0 kPa at 20C; and 4.0 kPa at 25C (Figs. 3 and 6). Insufficient data were available to estimate the RQ breakpoint at 0C, although it did not appear to be higher than for 5C. The RQ at higher, aerobic  $O_2$  partial pressures was  $\approx 1.3$  for all temperatures.

### Discussion

Storage temperature is known to affect the gaseous composition of MAP systems for various commodities (Kader et al., 1989), although in some cases the effect is rather minimal (Prince et al., 1986). It is recognized that steady-state  $O_2$  and  $CO_2$  levels depend on film permeability and product respiration and that the temperature dependence of these two processes is determined by film type, and commodity physiology, respectively. Additionally, suppression of respiration for some fruit takes place at  $CO_2$  levels above 10 to 20 kPa, but to our knowledge, this has not been documented for blueberry fruit. We therefore assumed respiration was minimally affected by levels of  $CO_2$  below the approximate 20 kPa that accumulated in packages under hypoxic conditions. This assumption has since been verified (R.M.B., unpublished).

The safe range of  $O_2$  partial pressures needs to be identified for any product if a MAP system is to be used. One measure of the lower  $O_2$  partial pressure limit is the lowest  $O_2$  partial pressure that does not induce anaerobic  $CO_2$  production. Anaerobic respiration can be detected by the upswing in the RQ (the RQ breakpoint) associated with the synthesis of acetaldehyde, ethanol, and  $CO_2$ . Although some degree of anaerobiosis can be tolerated (Cohen et al., 1990; Ke and Kader, 1990), there would be less risk if products were maintained at an  $O_2$  level higher than that associated with the RQ breakpoint. The RQ is easily calculated for fruit in MAP systems (Cameron, 1990; Cameron et al., 1989) and its breakpoint can be correlated with the package  $O_2$  partial pressure. For blueberry fruit, we have assumed the lower limit for the storage  $O_2$  partial pressure to be that partial pressure associated with the RQ breakpoint.

The rise in the lower  $O_2$  limit with increasing temperature has not been previously reported. This observed change can be explained, at least in part, in terms of gas diffusion into the fruit. For many fruits, resistance to  $O_2$  movement into the tissues is highest at the skin (Burg and Burg, 1965; Cameron and Yang, 1982). We hypothesize that as temperature increased, the rate of  $O_2$  consumption by the tissue rose more rapidly than skin permeability to  $O_2$ . For fruit with similar internal  $O_2$  levels (e.g., that internal  $O_2$  level which begins to induce fermentation), the  $O_2$  gradient across the skin would have increased as temperature increased, leading to the observed rise in steady-state  $O_2$  at the RQ breakpoint. The magnitude of the skin's permeability to either  $O_2$  or  $CO_2$  and the temperature sensitivity of these permeabilities are unknown.

The high RQ ( $\approx 1.3$ ) of aerobic fruit might be indicative of the oxidation of organic acids. Both organic acids (mostly citric acid) and sugars are plentiful in blueberry fruit, commonly reaching levels of 0.3% to 1.3% and 12% to 15%, respectively (Eck, 1988).

The possibility of creating hypoxic environments within MAP systems during handling, transit, and storage is a serious concern for commercial enterprises interested in using MAP techniques, especially with regard to temperature fluctuations. The data indicate that a MAP system for blueberry fruit, designed to develop and maintain aerobic steady-state  $O_2$  partial pressures

for storage temperatures ranging from 0 to 25C, should maintain an  $O_2$  partial pressure at or above  $\approx 4$  kPa at 25C and at or above  $\approx 1.8$  kPa at 0C. If the goal of MAP of blueberry fruit were to maintain these minimal  $O_2$  levels, then the LDPE film used here would not be appropriate. For example, when optimizing packages for storage at 0C, about 110 g fruit weight per package achieved an  $O_2$  partial pressure near the lowest tolerable level of  $\approx 1.8$  kPa (Fig. 3). These same 110-g packages were clearly hypoxic at 25C, the fruit having an RQ of  $\approx 3$ .

To maintain the lowest  $O_2$  partial pressures tolerable at all temperatures for blueberry fruit would require a film whose  $O_2$  permeability would increase more rapidly with temperature than that of LDPE. In this experiment, the decline in steady-state  $O_2$  for a given fruit weight with increasing temperature indicated that  $O_2$  consumption was more sensitive to temperature than  $O_2$  permeation through the LDPE film. A film with a greater temperature sensitivity than LDPE would need to have an energy of activation for  $O_2$  permeability higher than the  $40 \text{ kJ}\cdot\text{mol}^{-1}$  for LDPE. To our knowledge, films with higher energies of activation for  $O_2$  permeation all have very low  $O_2$  permeability.

An enhancement of storage life of blueberry fruit by low  $O_2$  is open to question in that decay is often the primary determinant of blueberry fruit shelf life. Ceponis and Cappellini (1985) found that CA storage of highbush blueberry fruit at 2 kPa  $O_2$  and 2C did not effectively reduce the incidence of decay relative to air, nor did it enhance the effect of  $CO_2$  treatment. However, the storage period was relatively short (7 to 14 days) in comparison to the potential storage life of blueberry fruit (35 to 40 days) (Bunemann et al., 1957; Hruschka and Kushman, 1963). In other studies, storage of highbush blueberry fruit under low  $O_2$  (1.5 to 2 kPa) at nonfungistatic  $CO_2$  partial pressures suggests that low  $O_2$  was helpful in reducing the incidence of runny and decayed berries during long-term storage (5 to 7 weeks) (Frisina et al., 1988; D.L.D. and R. M. B., unpublished data; Dilley, unpublished data).

The methodology outlined here would be useful in defining the lower  $O_2$  limits for numerous commodities. Furthermore, it can be used to generate the data necessary to establish film permeability characteristics needed for developing a working MAP system that would avoid anaerobic atmospheres. A model that can be used to specifically determine the needed temperature sensitivity of a film's  $O_2$  permeability has been developed for blueberry fruit using these respiration data (A.C.C. and R. M. B., unpublished).

Developing a functional and practical MAP system for any perishable commodity requires that we understand how temperature affects film permeability characteristics, the respiratory processes of  $O_2$  consumption and  $CO_2$  production, and the lower  $O_2$  limit. Additional progress needs to be made in the areas of film manufacture, packing techniques, package construction, handling, and marketing to make MAP of blueberry or other commodities a viable alternative to either CA storage or the simple overwraps presently used.

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